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**(54) Production and use of open cell rigid polyurethane foam**

Herstellung und Verwendung von offenzelligen Polyurethanhartschäumen

Production et utilisation de mousse de polyuréthane rigide à cellules ouvertes

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**EP 0 581 191 B1**

**Description**Field of the Invention

5 This invention relates to production and use of an open cell rigid polyurethane foam, and more particularly, to a method for the production of an open cell rigid polyurethane foam by use of a substitute for trichlorofluoromethane as a blowing agent, and use of such a foam as a heat insulating material.

Background of the Invention

10 A closed cell rigid polyurethane foam is a good heat insulating material having excellent moldability and processability, and is in wide use as a heat insulating material in refrigerators, buildings, low temperature warehouses, storage tanks, refrigerator ships, or pipings. The rigid foam has been improved in thermal conductivity year by year, and has at present a value of 0.015 W/mK on a commercial basis. Thus, it is said that the rigid polyurethane foam has the  
 15 smallest thermal conductivity of the heat insulating materials presently used around normal temperatures. Nevertheless, further reduction of thermal conductivity is increasingly demanded.

For the production of a closed cell rigid polyurethane foam, a one shot method is usually employed wherein an A component mainly composed of a polyol, a catalyst, a foam stabilizer and a blowing agent and a B component mainly composed of an organic polyisocyanate are mixed together so that the components react to carry out a foaming process  
 20 and a curing process in parallel, thereby to form a foam.

Among the blowing agents used in the production of such a closed cell rigid polyurethane foam, trichlorofluoromethane or R-11 is well known. However, the conventional chlorofluorocarbons (CFC's) exemplified by R-11 are chemically stable so that they diffuse into the stratosphere to destroy the ozone layer. As results, the solar ultraviolet radiation is not absorbed by the ozone layer, but it reaches the surface of the earth, and is causing a global environmental problem. For this reason, the use of CFC's has been limited since 1989, and the use of R-11 for the production  
 25 of polyurethane foam as well.

Under those circumstances, the investigation of a substitute as a new blowing agent for the conventional chlorofluorocarbons has been made, and for example, 1,1-dichloro-1-fluoroethane (referred to as HCFC-141b hereinafter) or methylene chloride are put up as a candidate of a substitute for R-11.

30 However, in general, the heat conductivity of a heat insulating material composed of a closed cell rigid polyurethane foam can not be made smaller than that of a blowing agent used in the production of the foam, so that it is almost impossible to produce a closed cell rigid polyurethane foam having such a small heat conductivity as has been hitherto achieved if a substitute for R-11 must be used as a blowing agent.

Thus, a vacuum heat insulating material has been recently given attention again which is composed of a core  
 35 material enclosed in a vacuum container of metal-plastic laminate film, as disclosed in Japanese Patent Application Laid-open No. 64-4112.

There are already known two kinds of core materials for use in vacuum heat insulating materials. One is an inorganic material such as perlite, and the other is an organic material such as an open cell polyurethane foam. The inorganic material is inferior in workability to the organic material, and in addition, it is of a high density and cost. On the other hand, an open cell rigid polyurethane foam is free from such problems as above involved in the use of inorganic core material. However, it is required that the open cell rigid polyurethane foam has cells of very small size in order to retain  
 40 such a low thermal conductivity as required over a long period of time, since when an open cell rigid polyurethane foam is used as a core material, the thermal conductivity of the resultant vacuum heat insulating material is largely dependent upon the cell size.

45 As the average cell size is taken as an average of major axis and minor axis of cells of foam, the conventional open cell rigid polyurethane foam has an average cell size of 300-1000  $\mu\text{m}$ . Accordingly, it is necessary to make the inside of the foam reach to such a high level of vacuum of about 0.133 Pa (0.001 mmHg) in order to obtain a high performance vacuum heat insulating material. However, it needs infeasibly much time to make such an open cell rigid polyurethane foam having an average cell size of about 300-1000  $\mu\text{m}$  vacuous to such a high level of vacuum as above  
 50 stated. Thus, it is necessary that an open cell rigid polyurethane foam has an average cell size of not more than 250 microns to reduce the influence of thermal conduction by gas sufficiently by making the inside of the foam vacuous at a readily attainable level of vacuum of 13.3 Pa - 1.33 Pa (0.1-0.01 mmHg).

It is also an important requisite that the open cell rigid polyurethane foam has no closed cells. When the foam has the slightest amount of closed cells, the vacuum heat insulating material containing such a foam as a core material is  
 55 greatly reduced in heat insulating performance if the material has an excellent heat insulation at the initial stage, since the blowing gas enclosed in the closed cells escapes from the cells gradually into the vacuum heat insulating material as time passes so that the pressure inside the vacuum heat insulating material rises accordingly.

For instance, presume that an open cell rigid polyurethane foam has a volume of 1800  $\text{cm}^3$  and closed cells in an

amount of 2%, and that a vacuum heat insulating material is manufactured which has a thermal conductivity of about 5 mW/mK by making the inside of the foam reach to a level of vacuum of 0.133 Pa (0.001 mmHg). The resultant vacuum heat insulating material contains about 36 cm<sup>3</sup> of gas in the closed cells, and the gas gradually diffuses into the vacuous open cells against the diffusion resistance of cell walls of the closed cells, and accordingly the pressure inside the vacuum heat insulating material rises to a level of 1999 Pa (15 mmHg), and the thermal conductivity is reduced to about 23 mW/mK or more.

If any, such closed cells are contained concentratedly in the skin layer of open cell rigid polyurethane foam. Thus, from the standpoint of raising the yield rate of products, it is necessary to produce a large block of foam, and make the rate of skin layer to the volume of the block as small as possible as the skin layer is removed from the block when it is put to use. However, the production of a large block of open cell rigid polyurethane foam is attended by a difficulty. Namely, while an open cell rigid polyurethane foam is formed, the resulting foam has a temperature as high as about 200°C or more inside the foam, and the air readily penetrates deeply into the resultant foam where such a high internal temperature is reached, so that it usually takes place that the resultant open cell rigid polyurethane foam readily carbonizes. Thus, the resultant foam readily scorches.

#### Brief Summary of the Invention

It is, therefore, an object of the invention to provide a method of producing an open cell rigid polyurethane foam, even a large size one with no scorching or burning, which has cells of much smaller size and hence a much smaller thermal conductivity than the conventional open cell rigid polyurethane foam.

The invention provides a method of producing an open cell rigid polyurethane foam which comprises reacting a polyol with a polymethylene polyphenyl polyisocyanate prepolymer with a monol by use of a substitute for trichlorofluoromethane as a blowing agent in the presence of a catalyst, a foam stabilizer and a cell opening agent.

#### Detailed Description of the Invention

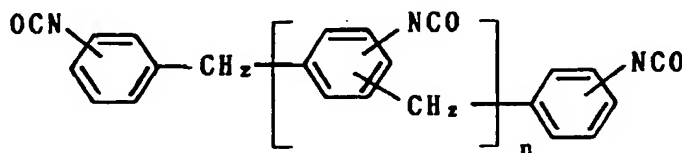
The present invention relates to a method of producing an open cell rigid polyurethane foam which comprises: reacting a polyether polyol having a functionality of 2 to 8 and a hydroxyl value of 300 to 450 mg KOH/g with a polymethylene polyphenyl polyisocyanate prepolymer obtained by the reaction of polymethylene polyphenyl polyisocyanate with a monol, at an NCO/OH equivalent ratio of 1.3 to 3.0 by use of a blowing agent which is at least one volatile blowing agent selected from the group consisting of hydrochlorofluorocarbons of one or two carbons, hydrofluorocarbons of two to four carbons, perfluorocarbons of four to six carbons, methylene chloride, pentane cyclopentane and chloropentane, or a mixture of the said at least one volatile blowing agent with water, in the presence of a catalyst, a foam stabilizer and a cell opening agent.

Further the present invention relates to an open cell rigid polyurethane foam obtainable according to the method mentioned above and to a vacuum heat insulating material which comprises said open cell rigid polyurethane foam enclosed in a metal plastic laminate film under vacuum.

The polyol used in the invention may be any polyfunctional polyol which has been used in the production of conventional rigid polyurethane foam.

Most preferred is a polyether polyol which is obtained as an addition product of ethylene oxide or propylene oxide or both to one or a mixture of polyfunctional compounds containing active hydrogens therein such as a polyhydric alcohol, e.g., trimethylolpropane or sorbitol, or such as a polyfunctional amine compound, e.g., ethylenediamine, o-tolenediamine or m-tolenediamine, and which has a hydroxyl value of 300-450 mg KOH/g.

The polymethylene polyphenyl polyisocyanate prepolymer with a monol used in the invention is obtained by the reaction of a polymethylene polyphenyl polyisocyanate of the formula



wherein n is an integer of 0-10, which is commercially available, with a monol or a monohydric alcohol, and has an amine equivalent preferably of 140-200.

The monol used in the production of prepolymer includes, for example, an alcohol such as methanol, ethanol,

isopropanol, n-butanol, pentanol, hexanol, heptanol, octanol or phenylethyl alcohol; and a monoalkyl ether of (mono or poly)alkylene glycol such as ethylene glycol monomethyl ether, diethylene glycol monomethyl ether, triethylene glycol monomethyl ether, ethylene glycol monoethyl ether, diethylene glycol monoethyl ether, ethylene glycol monododecyl ether, ethylene glycol monoallyl ether, ethylene glycol monobenzyl ether, ethylene glycol mono-n-butyl ether, ethylene glycol mono- $\beta$ -chloroethyl ether, ethylene glycol mono-n-hexyl ether, ethylene glycol monoisopropyl ether, ethylene glycol monophenyl ether, diethylene glycol monododecyl ether, diethylene glycol mono- $\beta$ -chloroethyl ether, diethylene glycol monochlorohydrin, diethylene glycol mono-n-hexyl ether, diethylene glycol monoisobutyl ether, triethylene glycol monododecyl ether, triethylene glycol mono-n-butyl ether or triethylene glycol monochlorohydrin; and an addition product of alkylene oxides such as ethylene oxide, propylene oxide, butylene oxide or a mixture of these.

The monol may be used singly or as a mixture.

If necessary, other polyisocyanates or their prepolymers such as tolylene diisocyanate or its prepolymer may be used together with the polymethylene polyphenyl polyisocyanate prepolymer.

It is preferred that the polymethylene polyphenyl polyisocyanate prepolymer is reacted with a polyol at an NCO/OH equivalent ratio or isocyanate index of 1.5-2.5.

The substitute for trichlorofluoromethane used as a blowing agent according to the invention is a volatile blowing agent or chemically inactive blowing agent which does not chemically participate in blowing or is not chemically involved in blowing. Such volatile blowing agents are hydrochlorofluorocarbons or alkanes of one or two carbons in which some of hydrogens are replaced by chlorine and fluorine atoms and which are relatively readily decomposed; hydrofluorocarbons or alkanes of two to four carbons which have no chlorine atoms therein, but have some fluorine atoms in place of hydrogens; and perfluorocarbons or alkanes of four to six carbons wherein all the hydrogens are replaced by fluorine atoms.

The hydrochlorofluorocarbon may be exemplified by, for example, HCFC-141b, 1-chloro-1,1-difluoroethane or chlorodifluoromethane; the hydrofluorocarbon may be exemplified by, for example, 1,1,1,2-tetrafluoroethane, 1,1,2,2,3-pentafluoropropane (hereinafter referred to as CFC-245), 1,1,1,2,3,3-hexafluoropropane (hereinafter referred to as CFC-236) or 1,1,1,4,4,4-hexafluorobutane (hereinafter referred to as CFC-356); and the perfluorocarbon may be exemplified by, for example, perfluoropentane or perfluorohexane.

The substitute for trichlorofluoromethane used as a volatile blowing agent in the invention can also be methylene chloride, pentane, cyclopentane, chloropentane or carbon dioxide, as carbon dioxide is herein included in the volatile blowing agent for convenience.

Preferably a small amount of water, known as a chemical blowing agent which generates carbon dioxide by the reaction with the polyisocyanate, may be used together with the volatile blowing agent as mentioned above.

Among a variety of the blowing agents as above mentioned is preferred in particular HCFC-141b, a combination of HCFC-141b with water, or a combination of methylene chloride with water.

The amount of the blowing agent is suitably selected so as to provide an open cell rigid polyurethane foam having a density of 25-100 kg/m<sup>3</sup>. More specifically, the volatile blowing agent may be used usually in an amount in the range of 5-150 parts by weight in relation to 100 parts by weight of polyols used. When water is used together with the volatile blowing agent, the water may be used in an amount of 0.1-10 parts by weight, preferably 0.1-3 parts by weight, in relation to 100 parts by weight of polyol used.

The reaction of a polyol with a polymethylene polyphenyl polyisocyanate is effected in the presence of a catalyst, a foam stabilizer and a cell opening agent.

A known isocyanurating catalyst is preferably used, which includes, for example, an amine catalyst such as 2,4,6-tris(dimethylaminomethyl)phenol, triethylamine, N,N',N"-tris(dimethylaminopropyl)hexahydrotriazine, triethylenediamine, diazabicycloundecene or tetramethylhexanediamine; a carboxylic acid alkali metal salt such as potassium acetate, potassium benzoate, potassium 2-ethylhexanoate or potassium naphthenate; a strongly basic metal hydroxide such as potassium hydroxide, sodium hydroxide or calcium hydroxide; an alcoholate or a phenolate such as potassium phenolate or sodium methoxide. The catalyst may be used singly or as a mixture.

The above catalyst may further be used together with a conventional catalyst used in the production of rigid polyurethane foams. The conventional catalyst may include, for example, a tertiary amine such as dimethylethanolamine, triethylenediamine, tetramethylethylenediamine, tetramethylpropylenediamine, tetramethylhexamethylenediamine or dimethylcyclohexylamine; an organometallic compound such as stannous octoate, dibutyltin dilaurate or lead octanoate; or a tertiary amine carboxylate.

The catalyst may be used in an amount of 0.01-20% by weight based on the amount of the polymethylene polyphenyl polyisocyanate prepolymer with a monol used.

The foam stabilizer used includes, for example, a silicone surfactant such as an organopolysiloxane, an organopolysiloxane-polyoxyalkylenecopolymer, a polyalkenylsiloxane having polyoxyalkylene side chains, and a fluorinated surfactant, a cationic, anionic or nonionic surfactant. The foam stabilizer may be used in an amount of 0.2-10% by weight based on the polyol used.

The cell opening agent used may be a known powdery divalent metal salt of a saturated carboxylic acid, preferably

a fatty acid, such as calcium stearate, magnesium stearate, strontium stearate, zinc stearate or calcium myristate, as disclosed in Japanese Patent Application Laid-open No. 61-153480, or a powder of a thermoplastic resin such as polyethylene, as disclosed in Japanese Patent Application Laid-open No. 61-153478. The cell opening agent may be used in an amount of 0.1-20% by weight based on the polyol used.

The above mentioned raw materials are evenly mixed together by use of, for example, a high pressure foaming machine, to readily provide an open cell rigid polyurethane foam whose cell size is very small with no scorching or burning.

As above set forth, the method of the invention readily provides an open cell rigid polyurethane foam having a very small cell size and a very large block size with no undesirable scorching or burning by use of a polymethylene polyphenyl polyisocyanate prepolymer with a monol as a polyisocyanate together with such a substitute for R-11 as a blowing agent. Furthermore, the foam has a complete open cell structure.

According to the invention, as set forth above, a polyol is reacted with a polymethylene polyphenyl polyisocyanate prepolymer with a monol by use of a substitute for trichlorofluoromethane as a blowing agent in the presence of a catalyst, a foam stabilizer and a cell opening agent, to provide an open cell rigid polyurethane foam having a cell size as small as about 200-250  $\mu\text{m}$ , and even a foam of a very large block size with no scorching attended. Thus, the open cell rigid polyurethane foam may be used advantageously as a core material in a vacuum heat insulating material. The foam may be enclosed in a container under a vacuum of 13.33-1.33 Pa (0.1-0.01 mmHg) readily attainable to provide a vacuum heat insulating material of a high heat insulating performance.

The invention provides a method of producing an open cell rigid polyurethane foam which comprises reacting a polyol with a polymethylene polyphenyl polyisocyanate prepolymer with a monol by use of a substitute for trichlorofluoromethane as a blowing agent in the presence of a catalyst, a foam stabilizer and a cell opening agent.

The invention will now be described in more detail with reference to examples and reference examples, however, the invention is not limited thereto.

#### Examples 1 to 5

The materials used in these examples and reference examples 1-5 are as follows:

Polyether polyol	Addition product of alkylene oxide to a mixture of tolylenediamine and ethylenediamine having a hydroxyl value of 450 mg KOH/g
Catalyst	Potassium acetate
Foam stabilizer	Silicone surfactant (F-373 available from Shin-etsu Kagaku Kogyo K.K.)
Blowing agent A	R-11
Blowing agent B	Water
Blowing agent C	HCFC-141b
Blowing agent D	Methylene chloride
Blowing agent E	HCFC-245
Blowing agent F	HCFC-356
Blowing agent G	Perfluoropentane
Cell opening agent	Calcium stearate
Polyisocyanate A	pMDI <sup>*)</sup>
Polyisocyanate B	Prepolymer obtained by the reaction of pMDI and bisphenol A, having an amine equivalent of 150.
Polyisocyanate C	Prepolymer obtained by the reaction of pMDI and bisphenol A, having an amine equivalent of 170
Polyisocyanate D	Prepolymer obtained by the reaction of pMDI and diethylene glycol monomethyl ether, having an amine equivalent of 170

<sup>\*)</sup> pMDI: polymethylene polyphenyl polyisocyanate

The materials as indicated in Table 1 were mixed together at temperature of  $25 \pm 1$  °C and reacted to form an open cell rigid polyurethane foam. The following day the resultant foam was cut to measure the cell size based on electromicrophotographs. The results are indicated in Table 1. The viscosity of polyisocyanate used at 25°C is also indicated in Table 1.

The resultant rigid foam was heated for about two hours at 120°C to remove moisture and unreacted materials therefrom, and was then enclosed in a laminate composed of metal and aluminum deposited polyester film/polyethylene film under a vacuum of 6.67 Pa (0.05 mmHg), thereby to provide a vacuum heat insulating material. The thermal

conductivity of the vacuum heat insulating material is indicated in Table 1.

#### Reference Examples 1-5 (not according to the invention)

In the same manner as in the example 1, the reaction was effected. The results are indicated in Table 1.

The reference example 1 effected the reaction of polymethylene polyphenyl polyisocyanate with a polyol in the presence of R-11 as a blowing agent. The resultant open cell rigid foam was found to have an average cell size as large as 350  $\mu\text{m}$ . The vacuum heat insulating material manufactured by use of the foam as a core material was found to have a thermal conductivity of  $81 \times 10^{-4} \text{ W/mK}$ .

It is necessary that an open cell rigid polyurethane foam has an average cell size of not more than 250  $\mu\text{m}$  in order to obtain a practical vacuum heat insulating material having a thermal conductivity of not more than  $64 \times 10^{-4} \text{ W/mK}$ , preferably not more than  $58 \times 10^{-4} \text{ W/mK}$ .

In the reference example 2, a polymethylene polyphenyl polyisocyanate prepolymer with a bisphenol A (having an amine equivalent of 150) was used in place of polymethylene polyphenyl polyisocyanate, and the reaction was effected otherwise in the same manner as in the reference example 1. The resultant open cell rigid foam was found to have a reduced average cell size of 300  $\mu\text{m}$ . The vacuum heat insulating material having the foam as a core material incorporated therein was also found to have a reduced thermal conductivity of  $70 \times 10^{-4} \text{ W/mK}$ , which was then found to be still unsatisfactory.

It would be expected that the use of a polyisocyanate having a higher amine equivalent provides an open cell rigid polyurethane foam having a smaller cell size. However, as noted from the reference example 3 wherein a polymethylene polyphenyl polyisocyanate prepolymer with a diol such as bisphenol A, the viscosity of the prepolymer used became larger as the amine equivalent became higher. For example, the prepolymer having an amine equivalent of 170 had a viscosity of 7000 Pas at 25°C so that it could not be handled by a conventional high pressure foaming machine.

As further noted from the reference examples 4 and 5, the use of a polymethylene polyphenyl polyisocyanate prepolymer with a diol such as bisphenol A was found to fail to provide an open cell rigid polyurethane foam having a sufficiently small cell size and a thermal conductivity even if such a blowing agent as HCFC-141b or methylene chloride was used.

In contrast, the use of a polymethylene polyphenyl polyisocyanate prepolymer with monool according to the invention readily provided an open cell rigid polyurethane foam having an average cell size of about 200  $\mu\text{m}$  by use of a conventional foaming machine since the prepolymer had a small viscosity. Furthermore, the use of the thus obtained open cell rigid polyurethane foam readily provided a vacuum heat insulating material having a thermal conductivity of  $58 \times 10^{-4} \text{ W/mK}$ .

#### Examples 6 to 11

The materials used in these examples and reference examples 6-9 are as follows:

Polyol A	Addition product of alkylene oxide to a mixture of tolylenediamine and ethylenediamine, having a hydroxyl value of 475 mg KOH/g
Polyol B	Addition product of alkylene oxide to a mixture of tolylenediamine and ethylenediamine, having a hydroxyl value of 450 mg KOH/g
Polyol C	Addition product of alkylene oxide to a mixture of tolylenediamine and ethylenediamine, having a hydroxyl value of 375 mg KOH/g
Polyol D	Addition product of alkylene oxide to a mixture of tolylenediamine and ethylenediamine, having a hydroxyl value of 300 mg KOH/g
Polyol E	Addition product of alkylene oxide to a mixture of tolylenediamine and ethylenediamine, having a hydroxyl value of 275 mg KOH/g
Catalyst	Potassium acetate
Foam stabilizer	Silicone surfactant (F-373 available from Shin-etsu Kagaku Kogyo K.K.)
Blowing agent	HCFC-141b
Cell opening agent	Calcium stearate
Polyisocyanate	Prepolymer obtained by the reaction of polymethylene polyphenyl polyisocyanate and diethylene glycol monomethyl ether, having an amine equivalent of 170

The materials as indicated in Table 2 were mixed together at temperature of  $25 \pm 1^\circ\text{C}$  and reacted to form an open cell rigid polyurethane foam in a wooden box of 400 mm cube with use of high pressure foaming machine, while the

internal temperature at the central part of the resultant foam was measured. After the internal temperature of the foam reached room temperature, the internal part of the foam was cut away to check if there took place scorching. The results are indicated in Table 2.

5 Reference Examples 6 to 9 (not according to the invention)

In the same manner as in the examples 6-11, the reaction was effected using the materials indicated in Table 2. In some of the reference examples, the materials were foamed in a wooden box of 100 mm cube (i.e., block size of 100 mm cube) with use of high pressure foaming machine. The results are indicated in Table 2.

10 The reference example 6 effected the reaction of a polyol A having a hydroxyl value of 475 mg KOH/g at an NCO/OH equivalent ratio or isocyanate index of 1.0 in a wooden box of 100 mm cube. The resultant foam was found to have no scorching, however, since the reaction was effected at a small value of isocyanate index, the resultant foam was found to be insufficient in strength.

15 A rigid foam which has an insufficient strength as above mentioned is contracted and deformed when it is evacuated, to fail to provide a vacuum heat insulating material. A rigid foam for use as a core material in a vacuum heat insulating material is therefore required to have a sufficient strength.

The reference example 7 effected the reaction in the same manner as in the example 11 (not according to the invention) except that the resultant foam had a block size of 400 mm cube. The foam was found to be attended by scorching to some degree presumably because of a larger block size of foam and hence a larger amount of heat accumulated in the foam to accelerate carbonizing reaction in the foam.

20 However, as illustrated in the example 6, the use of polyol B having a hydroxyl value of 450 mg KOH/g at an isocyanate index of 2.0 provided a rigid foam of a block size of 400 mm cube, as in the case of the example 11. Accordingly, as will be clearly seen from the comparison of the examples 6 and 11 with the reference example 7, it is necessary to use a polyol having a hydroxyl value of not more than 450 mg KOH/g in order to produce a rigid foam of a large block size.

25 As further illustrated in the examples 7, 8 and 9, the use of polyol having a hydroxyl value of 375 mg KOH/g provided a rigid foam of excellent properties with no scorching either at an isocyanate index of 1.3 or 2.0 or 3.0. However, as indicated in the reference example 8, when the reaction was effected at an isocyanate index of 1.0, a rigid foam was obtained with no scorching, but the foam was of insufficient strength.

30 As will be apparent from the example 10, the use of polyol D having a hydroxyl value of 300 mg KOH/g provided a rigid foam of excellent properties. However, as seen in the reference example 9, when a polyol having a more reduced hydroxyl value (to a level of 275 mg KOH/g) was used, the heat generated was also reduced so that the resultant foam had no scorching, but had an insufficient strength as in the case of the reference example 8.

TABLE 1

	EXAMPLES					REFERENCE EXAMPLES				
	1	2	3	4	5	1	2	3	4	5
FORMULA (parts by weight)										
Polyol	100	100	100	100	100	100	100	100	100	100
Catalyst	1	1	1	1	1	1	1	1	1	1
Foam stabilizer	2	2	2	2	2	2	2	2	2	2
Blowing agent A	0	0	0	0	0	15	15	15	0	0
Blowing agent B	1.5	1.5	1.5	1.5	2.0	1.5	1.5	1.5	1.5	1.5
Blowing agent C	14	0	0	0	0	0	0	0	14	0
Blowing agent D	0	10	0	0	0	0	0	0	0	10
Blowing agent E	0	0	11	0	0	0	0	0	0	0
Blowing agent F	0	0	0	12	0	0	0	0	0	0
Blowing agent G	0	0	0	0	15	0	0	0	0	0
Cell opening agent	1	1	1	1	1	1	1	1	1	1
Polyisocyanate A	0	0	0	0	0	198	0	0	0	0
Polyisocyanate B	0	0	0	0	0	0	218	0	218	218
Polyisocyanate C	0	0	0	0	0	0	0	247	0	0
Polyisocyanate D	247	247	247	247	247	0	0	0	0	0
PRODUCTION OF FOAM										
Viscosity of										
Polyisocyanate (Pas)	1000	1000	1000	1000	1000	200	1000	7000	1000	1000
Isocyanate index	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
PROPERTIES OF FOAM										
Cell size ( $\mu\text{m}$ )	200	200	250	250	180	350	300	-	300	300
Thermal conductivity	58	58	58	64	52	81	70	-	70	70
( $\times 10^{-4} \text{ W/mK}$ )										



TABLE 2

	EXAMPLES								REFERENCE EXAMPLES			
	6	7	8	9	10	11**	6**	7**	8**	9**		
FORMULA (parts by weight)												
Polyol A	-	-	-	-	-	100	100	100	-	-	-	-
Polyol B	100	-	-	-	-	-	-	-	-	-	-	-
Polyol C	-	100	100	100	-	-	-	-	100	-	-	-
Polyol D	-	-	-	-	100	-	-	-	-	-	-	-
Polyol E	-	-	-	-	-	-	-	-	-	100	-	-
Catalyst	1.3	0.9	1.2	1.6	1.0	1.4	0.9	1.4	0.8	0.9	-	-
Foam stabilizer	2	2	2	2	2	2	2	2	2	2	-	-
Blowing agent	43	29	38	51	33	45	29	45	25	31	-	-
Cell opening agent	1	1	1	1	1	1	1	1	1	1	-	-
Polyisocyanate	273	148	227	341	182	288	144	288	114	167	-	-
PRODUCTION OF FOAM												
Hydroxyl value (mg KOH/g)	450	375	375	375	300	475	475	475	375	275	-	-
Isocyanate index	2.0	1.3	2.0	3.0	2.0	2.0	1.0	2.0	1.0	2.0	-	-
Block size (mm cube)	400	400	400	400	400	100	100	400	400	400	-	-
Internal temperature (°C)	190	174	175	176	160	182	180	-	174	155	-	-
PROPERTIES OF FOAM												
Cell size (µm)	200	250	200	250	200	200	250	-	250	200	-	-
Thermal conductivity (x 10 <sup>-4</sup> W/mK)	58	64	58	64	58	58	-	-	-	-	-	-
Scorching	S*	No	No	No	No	S*	No	Yes	No	No	-	-
Strength of foam	Good	Good	Good	Good	Good	Good	Poor	-	Poor	Poor	-	-

\*\* : not according to the invention

S\* : Slightly

## Claims

1. A method of producing an open cell rigid polyurethane foam which comprises: reacting a polyether polyol having a functionality of 2 to 8 and a hydroxyl value of 300 to 450 mg KOH/g with a polymethylene polyphenyl polyisocyanate prepolymer obtained by the reaction of polymethylene polyphenyl polyisocyanate with a monol, at an NCO/OH equivalent ratio of 1.3 to 3.0 by use of a blowing agent which is at least one volatile blowing agent selected from the group consisting of hydrochlorofluorocarbons of one or two carbons, hydrofluorocarbons of two to four carbons, perfluorocarbons of four to six carbons, methylene chloride, pentane, cyclopentane and chloropentane, or a mixture of the said at least one volatile blowing agent with water, in the presence of a catalyst, a foam stabilizer and a cell opening agent.
2. The method as claimed in claim 1 wherein the hydrochlorofluorocarbon is 1,1-dichloro-1-fluoroethane, 1-chloro-1,1-difluoroethane or chlorodifluoromethane.
3. The method as claimed in claim 1 wherein the hydrofluorocarbon is 1,1,1,2-tetrafluoroethane, 1,1,2,2,3-pentafluoropropane, 1,1,1,2,3,3-hexafluoropropane or 1,1,1,4,4,4-hexafluorobutane.
4. The method as claimed in claim 1 wherein the perfluorocarbon is perfluoropentane or perfluorohexane.
5. The method as claimed in claim 1 wherein the blowing agent is at least one of 1,1-dichloro-1-fluoroethane and methylene chloride, or a mixture of water and at least one of 1,1-dichloro-1-fluoroethane and methylene chloride.
6. The method as claimed in claim 1 wherein the blowing agent is used in an amount of 5-150 parts by weight in relation to 100 parts by weight of the polyol.
7. The method as claimed in claim 1 wherein the polymethylene polyphenyl polyisocyanate prepolymer with a monol has an amine equivalent of 140 to 200.
8. The method as claimed in claim 7 wherein the polymethylene polyphenyl polyisocyanate prepolymer with a monol is a polymethylene polyphenyl polyisocyanate prepolymer with diethylene glycol monoalkyl ether.
9. The method as claimed in claim 1 wherein the polymethylene polyphenyl polyisocyanate prepolymer with diethylene glycol monoalkyl ether is reacted with a polyether polyol having a hydroxyl value of 300 to 450 mg KOH/g at an NCO/OH equivalent ratio of 1.3 to 3.0 by use of at least one member selected from the group consisting of 1,1-dichloro-1-fluoroethane, 1,1,2,2,3-pentafluoropropane, 1,1,1,2,3,3-hexafluoropropane, perfluoropentane and methylenechloride, or a mixture of said at least one member and water.
10. The method as claimed in claim 1 wherein the cell opening agent is an alkaline earth metal salt or a zinc salt of a fatty acid, or a powder of thermoplastic resin.
11. The method as claimed in claim 10 wherein the alkaline earth metal salt of a fatty acid is calcium stearate.
12. An open cell rigid polyurethane foam obtainable by the process according to any one of claims 1 to 11.
13. A vacuum heat insulating material which comprises the open cell rigid polyurethane foam according to claim 12 enclosed in a metal-plastic laminate film under vacuum.

## Patentansprüche

1. Verfahren zur Herstellung eines offenzelligen Polyurethanhartschaums, umfassend: das Umsetzen eines Polyetherpolyols mit einer Funktionalität von 2 bis 8 und einem Hydroxylwert von 300 bis 450 mg KOH/g mit einem Polymethylenpolyphenylpolyisocyanat-Prepolymer, das durch die Reaktion von Polymethylenpolyphenylpolyisocyanat mit einem Monol erhalten wurde, in einem NCO/OH-Äquivalentverhältnis von 1,3 bis 3,0 unter Verwendung eines Treibmittels, bei dem es sich um wenigstens ein flüchtiges Treibmittel, das aus der Gruppe ausgewählt ist, die aus Chlorfluorkohlenwasserstoffen mit einem bis zwei Kohlenstoffatomen, Fluorkohlenwasserstoffen mit zwei bis vier Kohlenstoffatomen, Perfluorkohlenstoffen mit vier bis sechs Kohlenstoffatomen, Methylenchlorid, Pentan, Cyclopentan und Chlorpentan besteht, oder ein Gemisch des wenigstens einen flüchtigen Treibmittels mit Wasser

handelt, in Gegenwart eines Katalysators, eines Schaumstabilisators und eines Zellöffnungsmittels.

2. Verfahren gemäß Anspruch 1, wobei es sich bei dem Chlorfluorkohlenwasserstoff um 1,1-Dichlor-1-fluorethan, 1-Chlor-1,1-difluorethan oder Chlordifluormethan handelt.
3. Verfahren gemäß Anspruch 1, wobei es sich bei dem Fluorkohlenwasserstoff um 1,1,1,2-Tetrafluorethan, 1,1,2,2,3-Pentafluorpropan, 1,1,1,2,3,3-Hexafluorpropan oder 1,1,1,4,4,4-Hexafluorbutan handelt.
4. Verfahren gemäß Anspruch 1, wobei es sich bei dem Perfluorkohlenstoff um Perfluorpentan oder Perfluorhexan handelt.
5. Verfahren gemäß Anspruch 1, wobei es sich bei dem Treibmittel um wenigstens einen der Stoffe 1,1-Dichlor-1-fluorethan und Methylenchlorid oder um ein Gemisch aus Wasser und wenigstens einem der Stoffe 1,1-Dichlor-1-fluorethan und Methylenchlorid handelt.
6. Verfahren gemäß Anspruch 1, wobei das Treibmittel in einer Menge von 5-150 Gewichtsteilen auf 100 Gewichtsteile des Polyols verwendet wird.
7. Verfahren gemäß Anspruch 1, wobei das Polymethylenpolyphenylpolyisocyanat-Prepolymer mit einem Monol ein Aminäquivalent von 140 bis 200 hat.
8. Verfahren gemäß Anspruch 7, wobei es sich bei dem Polymethylenpolyphenylpolyisocyanat-Prepolymer mit einem Monol um ein Polymethylenpolyphenylpolyisocyanat-Prepolymer mit Diethylenglycolmonoalkylether handelt.
9. Verfahren gemäß Anspruch 1, wobei das Polymethylenpolyphenylpolyisocyanat-Prepolymer mit Diethylenglycolmonoalkylether unter Verwendung wenigstens eines Vertreters aus der Gruppe, die aus 1,1-Dichlor-1-fluorethan, 1,1,2,2,3-Pentafluorpropan, 1,1,1,2,3,3-Hexafluorpropan, Perfluorpentan und Methylenchlorid besteht, oder eines Gemischs aus dem wenigstens einen Vertreter und Wasser mit einem Polyetherpolyol mit einem Hydroxylwert von 300 bis 450 mg KOH/g in einem NCO/OH-Äquivalentverhältnis von 1,3 bis 3,0 umgesetzt wird.
10. Verfahren gemäß Anspruch 1, wobei es sich bei dem Zellöffnungsmittel um ein Erdalkalimetallsalz oder ein Zinksalz einer Fettsäure oder ein Pulver aus einem thermoplastischen Harz handelt.
11. Verfahren gemäß Anspruch 10, wobei es sich bei dem Erdalkalimetallsalz einer Fettsäure um Calciumstearat handelt.
12. Offenzelliger Polyurethanhartschaum, der nach dem Verfahren gemäß einem der Ansprüche 1 bis 11 erhältlich ist.
13. Vakuumwärmeisoliermaterial, das den offenzelligen Polyurethanhartschaum gemäß Anspruch 12 umfaßt, der unter Vakuum in einer Metall-Kunststoff-Laminatschicht eingeschlossen ist.

#### Revendications

1. Procédé de production d'une mousse rigide en polyuréthane à cellules ouvertes, qui comporte le fait de faire réagir un polyétherpolyol, qui porte de 2 à 8 fonctions et dont l'indice d'hydroxyle vaut de 300 à 450 mgKOH/g, avec un prépolymère de polyméthylène-polyphényl-polyisocyanate obtenu par réaction d'un polyméthylène-polyphényl-polyisocyanate avec un monoalcool, en un rapport d'équivalents NCO/OH de 1,3 à 3,0 et en employant un agent d'expansion qui est constitué par au moins un agent volatil d'expansion choisi dans l'ensemble que constituent les hydrochlorofluorocarbures à 1-2 atomes de carbone, les hydrofluorocarbures à 2-4 atomes de carbone, les perfluorocarbures à 4-6 atomes de carbone, le chlorure de méthylène, le pentane, le cyclopentane et le chloropentane, ou qui est un mélange d'eau et d'au moins l'un de ces agents volatils d'expansion, en présence d'un catalyseur, d'un agent de stabilisation de mousse et d'un agent d'ouverture des cellules.
2. Procédé conforme à la revendication 1, dans lequel l'hydrochlorofluorocarbure est du 1,1-dichloro-1-fluoroéthane, du 1-chloro-1,1-difluoroéthane ou du chlorodifluorométhane.
3. Procédé conforme à la revendication 1, dans lequel l'hydrochlorofluorocarbure est du 1,1,1,2-tétrafluoroéthane,

du 1,1,2,2,3-pentafluoropropane, du 1,1,1,2,3,3-hexafluoropropane ou du 1,1,1,4,4,4-hexafluorobutane.

4. Procédé conforme à la revendication 1, dans lequel le perfluorocarbure est du perfluoropentane ou du perfluorohexane.
5. Procédé conforme à la revendication 1, dans lequel l'agent d'expansion est au moins l'un du 1,1-dichloro-1-fluoroéthane et du chlorure de méthylène, ou un mélange d'eau et d'au moins l'un du 1,1-dichloro-1-fluoroéthane et du chlorure de méthylène.
- 10 6. Procédé conforme à la revendication 1, dans lequel l'agent d'expansion est utilisé à raison de 5 à 150 parties en poids pour 100 parties en poids de polyol.
7. Procédé conforme à la revendication 1, dans lequel le prépolymère de polyméthylène-polyphényl-polyisocyanate et de monoalcool présente un équivalent amine de 140 à 200.
- 15 8. Procédé conforme à la revendication 7, dans lequel le prépolymère de polyméthylène-polyphényl-polyisocyanate et de monoalcool est un prépolymère de polyméthylène-polyphényl-polyisocyanate et d'éther monoalkylique de diéthylèneglycol.
- 20 9. Procédé conforme à la revendication 8, dans lequel on fait réagir le prépolymère de polyméthylène-polyphényl-polyisocyanate et d'éther monoalkylique de diéthylèneglycol avec un polyéther-polyol dont l'indice d'hydroxyle vaut de 300 à 450 mgKOH/g, en un rapport d'équivalents NCO/OH de 1,3 à 3,0 et en employant au moins l'un des éléments de l'ensemble que constituent le 1,1-dichloro-1-fluoroéthane, le 1,1,2,2,3-pentafluoropropane, le 1,1,1,2,3,3-hexafluoropropane, le perfluoropentane et le chlorure de méthylène, ou un mélange d'eau et d'au moins l'un de ces composés.
- 25 10. Procédé conforme à la revendication 1, dans lequel l'agent d'ouverture des cellules est un sel d'un métal alcalino-terreux ou de zinc et d'un acide gras, ou une résine thermoplastique en poudre.
- 30 11. Procédé conforme à la revendication 10, dans lequel le sel d'un métal alcalino-terreux et d'un acide gras est du stéarate de calcium.
12. Mousse rigide en polyuréthane à cellules ouvertes, que l'on peut préparer selon un procédé conforme à l'une des revendications 1 à 11.
- 35 13. Matériau d'isolation thermique sous vide, qui comporte une mousse rigide en polyuréthane à cellules ouvertes, conforme à la revendication 12, emballée sous vide dans un film de stratifié métal-plastique.